# CAN WEATHER DERIVATIVES BE IMPLEMENTED TO COVER VITICULTURE RELATED-RISKS? (REFEREED)

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#### Abstract

The management of weather-related risks is one of the main concerns of the farmers: the development of tools helping their risk covering of unfavourable climate seasons seems essential. This article is mainly focused on a financial contracts family: weather derivatives. The study tackles more specifically the wine-producing industry. The kind of weather-related risks the viticulturists are exposed to is first analyzed. The offer of weather derivatives which can be proposed by the market is also studied. A kind of product which can at the same time have a sufficient liquidity, and answer to the viticulturists needs, is inferred. In order to propose a pricing of these products, a simulation of the temperatures is realized. Determinist parameters of this simulation are estimated using an iterative method. Stochastic part is based on an autoregressive model with seasonal volatility, which parameters are estimated by the generalized least squares fitting method and which residual noise has been simulated by a numerical estimation of his inverse repartition function. The results of the study are presented for the products based on temperatures of Paris and Bordeaux.

### Introduction

The agricultural sector is confronted as all economical sectors to numerous risks, but it presents the particularity to be very exposed to weather-related risks. Farms can be affected in a very short time by significant losses of harvest and can be faced with a critical financial situation. Because of this, the management of weather-related risks is one of the main concerns of the farmers: the development of tools helping their risk covering of unfavorable climate seasons seems essential. During the last decades, numerous agricultural insurance programs have been tested and developed in several countries. Nevertheless, their range of application is limited to risks presenting at least some insurability characteristics. Moreover, considering obtained results of their implementing, some authors are questioning their efficiency, and suggest reviewing the range and the use of such programs (J.Skees, 2001;

S.Makko, 2002). In this context, new complementary tools should be developed. This article is mainly focused on a financial contracts family: weather derivatives. The study tackles more specifically the wine-producing industry, for which a future market has already been created in France (Winefex).

The kind of weather-related risks the viticulturists are exposed to is first analyzed. The offer of weather derivatives which can be proposed by the market is also studied. A kind of products which can at the same time have a sufficient liquidity, and answer to the viticulturists needs, is inferred. In order to propose a pricing of these products, a simulation of temperatures is realized. Determinist parameters of this simulation are estimated using an iterative method. Stochastic part is based on an autoregressive model with seasonal volatility, which parameters are estimated by the generalized least squares fitting method and which residual noise has been simulated by a numerical estimation of his inverse repartition function. The results of the study are presented for the products based on temperatures of Paris and Bordeaux.

#### I. WEATHER-RELATED RISK IMPORTANCE FOR VITICULTURISTS

Wine industry is facing many risks, regarding mostly quality and yield. Both characteristics remain largely defined by weather conditions.

#### I.1. Weather-related risk and crop quality

Objective criteria generally used to estimate crop quality are sugar, polyphenols content and acidity, mostly determined by photosynthesis phenomenon. Photosynthesis phenomenon depends on three weather characteristics: temperature, sunshine and pluviometry.

Temperature is considered in France as the main limiting factor of photosynthesis. This factor influences crop quality mainly during grape maturation phase. Between 18°C and 33°C (64,4°F - 91,4°F), photosynthesis efficiency reaches 90 to 100% (Kliewer, 1970), optimum being achieved circus 25°C (77,00°F) (Alleweldt & Ruehl, 1993). This efficiency heavily decreases beyond these temperature limits. Therefore, two types of temperature conditions that may be prejudicial to crop quality should be considered: too low temperatures during the whole maturation period, that could result in insufficiently sugared or too acid grapes; too high temperatures, that could generate insufficiently acid crops, and that may force viticulturists to bring forward harvest, and to realize it when temperature are still

high, which can be harmful to vinification process, specially for white wine. Specific vinification processes can correct some crop parameters: their impact on weather-related risk valuation will not be taken into account in this study.

Sunshine is also playing a significant role on crop quality, as it is one of the main factors of photosynthesis. The longer the sunshine during the vegetative period of grapevine, the more sugared and the less acid grapes will be. From this point of view, grapevine demands relatively luminous weather. Risk for crop quality is to receive insufficient sunshine, especially during maturation period. As sunshine is correlated with temperature, and its importance is less crucial than temperature under our latitudes, it won't be considered as a specific weather-related risk factor in this study.

Pluviometry has also its importance in grape quality: sugar-acidity-polyphenols relation is under dependence of considered terroir hydric regime. Best equilibrium is reached when grapevine is subjected to a rather humid weather (without any excess) till veraison (beginning in general at the end of July), to allow an optimal growth of the grapevine, and to a rather dry regime (without any excess) during maturation stage, to allow an optimal sugar accumulation in the berries, till the harvest generally conducted in September or October. In France, this factor presents a less important impact than temperature on grape quality; it mostly impacts yield.

#### I.2. Weather-related risk and yield

As for crop quality, weather conditions have a strong impact on yield. In this study, regulatory limits (defined for instance for French AOC, that have to comply with INAO decision), or voluntary limitations of yield will not be taken into account, as the goal of this study is exclusively weather-related risk.

Temperature has a direct effect on grapevine development and on yield. During winter, grapevine can cope with very low temperatures. From the end of flowering stage to the maturation period, temperature must reach a sufficient level (between 18°C to 25°C (64,40°F to 77,00°F)). Two main risks than can affect yield can be identified: frost and very high temperatures during a long period. Very strong frosts (below 5,00°F) can lead to partial or total destruction of stocks and roots; spring frosts can cause important damages after bud break. This risk will not be taken into account for two reasons: it can be limited by the use of agricultural processes<sup>1</sup> and can be insured. Finally, very high temperatures during an extended period can also

<sup>&</sup>lt;sup>1</sup> In areas particularly subject to frost, viticulturists have adapted grapevine work through specific techniques (artificial smoke clouds limiting temperature fall, late pruning...).

generate a lesser yield by leading to a "roasting" phenomenon and the drying out of the future crop.

Pluviometry also impacts yield. Rainfall levels from 400 to 600 millimeters per year represent ideal conditions for grapevine development. During winter, rains have no direct influence on the vineyard but allow the accumulation of water stocks that will be useful during spring and summer. At spring, rains are of great importance as grapevine growth depends on them. During summer, too high rainfall levels can lead to mildew development and threaten the crop. On the other hand, if hydric stock is insufficient, summer drought is also harmful to yield. These two risks are largely correlated with temperature risks mentioned further up (a rainy summer is generally cool, and a major drought is often accompanied by high temperatures). Researches in this paper are therefore limited to temperature risk study.

Fall rains happening before harvest may generate a development of grey mold and berry bursting. They can also hinder the harvest. Risks related to spring and fall rains are not being tackled in this paper. They may represent a valuable research path. Finally, hail risk can destroy in a few minutes a whole crop. As it can be insured, this risk will not be taken into account.

#### I.3. Main risks to be covered by weather derivatives

Two kinds of climatic risks could therefore be covered by weather derivatives: insufficient mean temperatures from the end of the flowering stage to the harvest and too high temperatures during maturation stage.

#### II. FORESEEABLE WEATHER DERIVATIVES OFFER IN THE MEDIUM TERM

Weather derivatives are rather illiquid products, today available on the Chicago Mercantile Exchange, and dealt as OTC products in France. Energy companies dominate this market. Two factors explain this domination:

- A volume effect: weather-related risk is massive due to heating and cooling energy sales (dozens of Euros billions in France in 2003<sup>2</sup>), that are extremely correlated to temperature.
- Their balanced cover needs, favoring market liquidity: two energy companies may seek an opposite position at the same time. Indeed, high summer

<sup>&</sup>lt;sup>2</sup> Household domestic energetic consumption reached Euros 35 billions in 2003 (« l'énergie en France – Repères » observatoire de l'énergie – MINEFI – édition 2004), and this consumption is for the most part linked to heating. Industrial and service energy consumption for heating purpose should also be added.

temperatures represent a risk for a company short in energy: these temperatures raise demand (higher air-conditioner consumption) and reduce some power plants capacities. On the other hand, they represent an opportunity for a "long" company (higher prices). Conversely, high winter temperatures represent an opportunity for a company short in energy and a risk for a "long" company: they reduce demand (lower heating related consumption) and therefore prices. A "short" energy company is to sell the weather derivative a "long" company is trying to buy.

Viticulturists, even if they decide to massively turn to weather derivatives, are to remain less important players in this market:

- Concerned volume is less important (11 Euros billions for the whole field in France)<sup>3</sup>.
- All viticulturists have to cover the same kind of risk, which would result in a completely illiquid viticulture-specific market. Indeed, viticulturists are to look for covers against too low mean temperatures during vegetative period cover or overly high temperature, specifically before harvest... Some nuances may exist, depending on vineyards characteristics, but they are to be traduced by different strike prices rather than by bullish or bearish positions regarding the same product.

Therefore, the following hypothesis is retained: viticulturists could not benefit from a specific weather derivatives offer but will have to cover their needs having recourse to the weather derivatives commonly traded on the energy market. These weather derivatives have the following characteristics:

- A mean daily temperature, computed from data gathered in one or several meteorological stations. These means can be computed from minimal and maximal temperature on a 24 hours period, or from several temperatures measured at regular intervals during 24 hours (the latter better corresponding to energy companies needs).
- > Degree days, computed as follows:
  - During summer : Max (mean daily temperature 18°C (~65°F) ; 0)
  - During winter : Min (mean daily temperature 18°C (~65°F); 0)
- > A period during which derivative is applied.
- > A strike, given in number of degree days on the period.
- > A tick, given in € per degree days, that allows the calculation of the pay-off.

<sup>&</sup>lt;sup>3</sup> AFP dispatch – December 7th 2004

- A pay-off, computed as follows: cumulated number of degree days above or below strike during the concerned period multiplied by tick.
- > A premium, fixed amount paid in advance by the derivative buyer.

# III. STUDIED WEATHER DERIVATIVES

In the previous chapter, it has been set that the weather derivatives structure to be studied should be inferred from energy products. Weather derivatives parameters described above are therefore to be fixed to answer viticulturists needs.

# III.1.Application period

In chapter 1, two major risks to be covered by viticulturists have been selected. These risks define an application period for related weather derivatives:

- Too cold temperatures from the end of flowering stage to the end of the maturation, corresponding to an application period from the 1<sup>st</sup> of July to the 30<sup>th</sup> of September.
- *Too high temperatures before the harvest*, corresponding to an application period from the 1<sup>st</sup> of August to the 15<sup>th</sup> of September<sup>4</sup>.

These periods may be adapted to answer specific needs, such as vineyard at altitude, or to adapt these derivatives for areas outside France.

# III.2. Choice and calculus of the underlying risk model

Application periods correspond to energy companies summer period. Underlying is therefore modeling using Cooling Degree Days, and is computed as:

 $\sum_{Application period} Max(mean \ daily \ temperature - 18^{\circ}C;0) \qquad (18^{\circ}C \sim 65^{\circ}C)$ 

Meteorological stations must be defined. Paris Montsouris and Bordeaux Mérignac have been chosen on the basis of following criteria:

- *Paris Montsouris* is the station the most likely to be chosen for the most liquid weather derivatives, therefore the most available for viticulturists. Indeed, liquidity is brought mainly by energy companies (cf. chapter II), and this station is representative of the most populated French area, and the one that use most energy. If the most liquid derivatives in France were to be based on a compound index made up from several different meteorological stations, weighting would be made notably from demographic criteria (corresponding to

<sup>&</sup>lt;sup>4</sup> High temperatures favour an early harvest.

the number of final clients), or from weather sensitive energy consumption. In both cases, Parisian area is to have the strongest weighting.

- Bordeaux Mérignac is a station representative of a major wine producing area, with a climate significantly different from Parisian area.

### III.3. Strike choice

Strike should have to be determined locally: depending whether the vineyard faces south, on wine production methods, on grape variety, each viticulturist will have to choose threshold beyond or over which yield or harvest quality is threatened. In fact, an expert will have to compute for each vineyard a threshold corresponding to a probability: for instance, the threshold corresponding to the coolest year in five years. Pricing study is therefore done choosing several strike levels.

### III.4. Tick value

Tick value has no direct impact on the method of calculation of weather derivatives (the higher the tick, the more selective this kind of product is for small concerns).

### IV. PRICING OF THE WEATHER DERIVATIVES STUDIED

Weather derivatives pricing has generated numerous papers. This pricing requires first to model temperature, then, from temperatures series, to model weather derivatives payoff, and finally, to infer corresponding premium.

# IV.1. <u>Temperature modeling</u>

### IV.1.1. Generic characteristics of temperature

From an intuitive comprehension of temperature, some characteristics are obvious:

- > temperature is a seasonal phenomenon,
- > temperature presents a several days correlation,
- temperature is stationary as a first approximation level.

These characteristics are the basis of all published temperature models, which can be brought together in two major types:

- mean-reversion models,
- autoregressive models.

IV.1.2. Two types of models presentation

# IV.1.2.1. Mean-reversion models

Alaton, Djehiche and Stillberger (2001) propose this kind of model, based on an initial model from Dischel (2000).

The model is a mean-reversion model, defined by:

$$dT_t = \left(\frac{d\theta_t}{dt} + \alpha(\theta_t - T_t)\right)dt + \sigma_t dW_t$$
 with:

 $\theta_t$  = Trend<sub>t</sub> + Seas<sub>t</sub>, the historical mean temperature for date t,

α, mean-reverting parameter,

 $\sigma_t$ , volatility,

W<sub>t</sub>, a standard brownian movement.

Temperature at a date t is therefore given by:

$$T_t = (T_0 - \theta_0)e^{-\alpha t} + \theta_t + \int_0^t e^{-\alpha(t-u)}\sigma_u dW_u$$

Barrieu (2002) has shown this model is not fully adapted to weather derivatives modeling:

- Model is extremely sensible to \_ parameter calculation. This heavily limits its reliability.
- Temperature time-series simulation through this kind of modeling produces results far from other considered modeling and above all far from historical trend.

# IV.1.2.2. Autoregressive models

These models are defined by:

 $T_t = Trend_t + Seas_t + Corr_t + R_t$  with:

Trend<sub>t</sub>, trend part of temperature, modeled as an time affine function with jumps, estimated on several years,

Seast, seasonal part of temperature,

Corr<sub>t</sub>, an AR(n) type process modeling correlation,

R<sub>t</sub>, model residual.

These models produce better results than mean-reverting ones. They are further studied in this article.

# IV.1.3. Temperature modeling

# IV.1.3.1. Determinist part estimation

A first study of series over 80 years (partially incomplete for Bordeaux Mérignac) highlights the nearly stationary characteristics of the series.



Though, five years moving average study shows a slight increase in mean yearly temperature.



- <u>Trend growth modeling</u>





An acceleration of this growth seems to occur in 1985-1988. Barrieu (2002) observes the same trend rupture in 1985 for Paris Montsouris series. A first factor is to be taken into account: a rise of mean yearly temperatures. As suggested in other published papers (Barrieu, 2002) the modeling of this rise is defined by an affine function with a jump:

$$Trend_{t} = \begin{cases} \alpha_{1}t + \beta_{1} & \forall t < t_{breakpoint} \\ \alpha_{2}t + \beta_{2} & \forall t \ge t_{breakpoint} \end{cases}$$

Breakpoint and <sub>1</sub> and <sub>2</sub> parameters will be computed globally with all other determinist parameters (cf. infra).

### - Seasonality modeling

Another factor to be taken into account in determinist modeling is seasonality. Seasonality can be clearly seen on 30 days minimum and maximum of daily temperatures.





To estimate this seasonality, "February 29<sup>th</sup>" are removed from the series to show yearly periodicity (Barrieu 2002; Diebold 2004).

Periodogram is computed using the following:

$$Periodogram(n) = \left| \sum_{k=0}^{N} T_k e^{i\frac{2k\pi n}{N}} \right| = \sqrt{\left( \sum_{k=0}^{N} T_k \cos\left(\frac{2k\pi n}{N}\right) \right)^2 + \left( \sum_{k=0}^{N} T_k \sin\left(\frac{2k\pi n}{N}\right) \right)^2} \text{ with } :$$

n, tested temperature function periodicity,

N, Sample size of data series (in this case 10950, corresponding to 30 years of daily data),

 $T_k$ ,  $k^{th}$  sample temperature.

Following results are obtained:





Two spikes are clearly observed for n=30 (3,88 for Paris Montsouris, 3,64 for Bordeaux Mérignac), corresponding to a yearly frequency, and for n = 60 (0,38 for Paris Montsouris, 0,47 for Bordeaux Mérignac) corresponding to a half-yearly frequency. Every other periodogram values are inferior or equal to 0,2.

Seasonal component is therefore modeled with a sum of yearly and half yearly sinusoids:

Seas<sub>t</sub>= a<sub>1</sub> cos(2 t/365)+ b<sub>1</sub> sin(2 t /365) + a<sub>2</sub> cos(4 t /365) + b<sub>2</sub> sin(4 t /365)

### - Trend and seasonal parameters estimation:

Following trend and seasonality parameters are computed:  $1, 1, 2, 2, t_{breakpoint}$ ,  $a_1, b_1, a_2, b_2$ . Proposed method to estimate these parameters is the following one:

- The series is first corrected from seasonal effects (computing of seasonal parameters a<sub>1</sub>, b<sub>1</sub>, a<sub>2</sub>, b<sub>2</sub>);
- Trend parameters 1, 1, 2, 2, t<sub>breakpoint</sub> are estimated from the series corrected from seasonal effects;
- Seasonal parameters a<sub>1</sub>, b<sub>1</sub>, a<sub>2</sub>, b<sub>2</sub> are re-estimated once seasonal effects removed.

This iterative methodology is designed to correct potential bias caused by border effects, that cannot be completely neglected as the period studied is only a few decades.

### 1<sup>st</sup> stage : initial correction of seasonal effect

Following expression is minimized function of a<sub>1</sub>, b<sub>1</sub>, a<sub>2</sub>, b<sub>2</sub>, using a Newton algorithm:

$$\left|T_{t} - Seas_{t}\right| = \sqrt{\sum_{t=0}^{N} \left(T_{t} - \left(a_{1}\cos\left(\frac{2\pi t}{365}\right) + b_{1}\sin\left(\frac{2\pi t}{365}\right) + a_{2}\cos\left(\frac{4\pi t}{365}\right) + b_{2}\cos\left(\frac{4\pi t}{365}\right)\right)\right)^{2}}$$

Following values are obtained:

|                       | Paris Montsouris | Bordeaux Mérignac |
|-----------------------|------------------|-------------------|
| a <sub>1</sub>        | -7,347           | -6,780            |
| b <sub>1</sub>        | -2,470           | -2,648            |
| <b>a</b> <sub>2</sub> | -0,021           | -0,121            |
| b <sub>2</sub>        | 0,759            | 0,932             |

# 2<sup>nd</sup> stage : Trend calculation

An empirical criterion is proposed to identify the breakpoint optimizing trend and time series adequacy. This criterion consists in minimizing the following function of 1, 1, 1,

2, 2 using a Newton algorithm for every  $t_{breakpoint} \in [1977/01/01; 2000/12/31]$ :

$$\left|T_{t}-Seas_{t}-Trend_{t}\right| = \sqrt{\sum_{t=0}^{t_{breakpoint}} \left(T_{t}-Seas_{t}-\alpha_{1}t-\beta_{1}\right)^{2} + \sum_{t=t_{breakpoint}+1}^{N} \left(T_{t}-Seas_{t}-\alpha_{2}t-\beta_{2}\right)^{2}}$$

For Paris:



For Bordeaux:



Minimum is reached for Paris and for Bordeaux on the 1<sup>st</sup> of August 1987.

Choice of the breakpoint has a limited impact on adequacy between trend and observed temperature: deviation remains important (about  $3^{\circ}C \sim 38^{\circ}F$ ), and varies very slightly whatever the breakpoint chosen. This deviation remains too important to

allow Chow test, for instance, to be conclusive on the validity of the breakpoint identified above.

The choice of this breakpoint has on the other hand a strong incidence on the resulting trend: if for instance trend had been estimated on the last ten years series, it would have been null, thus creating a deviation of  $0.2^{\circ}$ C (~  $32^{\circ}$ F) in 2003.

Obtained results are the following:

|                                                 | Paris Montsouris | Bordeaux Mérignac |
|-------------------------------------------------|------------------|-------------------|
| Trend 01/1974 – 07/1987                         | -0,047°C/an      | -0,011°C/year     |
| Trend 08/1987 – 12/2003                         | +0,027°C/an      | +0,040°C/year     |
| Jump of the trend on August <sup>1st</sup> 1987 | +1,071°C         | +1,094°C          |

These results highlight 1987 jump importance.

They also highlight linear modeling limits: slightly negative values observed on 74-87 period are negative, contrary to what could be observed on longer periods. Additional inquiry may be to use the results of physical modeling of the climate to precise this econometric approach oh the trend.

# <u>3<sup>rd</sup> stage : 2<sup>nd</sup> iteration of seasonal effects correction</u>

 $a_1$ ,  $b_1$ ,  $a_2$ ,  $b_2$  parameters are computed from  $T_t$  - Trend<sub>t</sub>, rather than from raw temperatures, to gain more precision in the estimation.

 $T_t$  - Trend<sub>t</sub> periodograms on the whole 1974-2003 period are more obvious than before: yearly and half-yearly spikes are better standing out.



Following results are obtained :

|                       | Paris M         | Iontsouris       | Bordeaux Mérignac             |        |  |
|-----------------------|-----------------|------------------|-------------------------------|--------|--|
|                       | After iteration | Before iteration | After itération Before iterat |        |  |
| <b>a</b> 1            | -7,352 (-0,08%) | -7,347           | -6,785 (-0,08%)               | -6,780 |  |
| b <sub>1</sub>        | -2,451 (+0,79%) | -2,470           | -2,620 (+1,04%)               | -2,648 |  |
| <b>a</b> <sub>2</sub> | -0,016 (+30,5%) | -0,021           | -0,116 (+4,42%)               | -0,121 |  |
| b <sub>2</sub>        | 0,761 (+0,25%)  | 0,759            | 0,937 (+0,60%)                | 0,932  |  |

# IV.1.3.2. Stochastic part estimation

To model stochastic part, data autocorrelogram should be studied first.

#### - Data autocorrelogram

Paris

#### Bordeaux

| 1 0.797 0.797 6960.4 0.000   2 0.583 0.145 10680 0.000   3 0.442 0.0172 12820 0.000   4 0.346 0.010 14132 0.000 3 0.400 0.054 1255 0.000   5 0.226 0.011 14955 0.000 5 0.2246 0.004 0.50 2.0.014 0.065 122.0 0.004 5 0.224.0 0.004 5 0.244 0.004 10 0.055 0.004 10 0.055 0.004 10 0.056 0.004 13.0 0.000 7 0.145 0.004 10 0.056 0.006 10 0.056 0.006 10 0.056 0.006 11 0.076 0.006 13.0 0.000 11 0.076 0.006 13.0 0.000 11 0.058 0.000 12 0.442 0.005 13.0 0.000 12 0.442 0.015                                                                                                                                                                                                                                  | Autocorrelation | Partial Correlation | AC       | PAC      | Q-Stat | Prob  | A | utocorrelation | Partial Correlation |      | AC     | PAC    | Q-Stat | Prob  |
|------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------|-----------------|---------------------|----------|----------|--------|-------|---|----------------|---------------------|------|--------|--------|--------|-------|
| 2 0.563-0.145 0.600 3 0.400 0.654 0.934 953.0 0.000   4 0.346 0.017 1282.0 0.000 3 0.400 0.654 1285.0 0.000   6 0.226 0.011 1495.0 0.000 6 0.192 0.023 0.000 6 0.192 0.005 13.04.0 0.001   7 0.185 0.000 7 0.185 0.000 7 0.145 0.014 36.0 0.000   9 0.120 0.012 1623 0.000 10 0.056 0.004 13.056 0.000   11 0.076 0.001 12 0.062 0.001 13.0034 0.000 13.0034 0.000 13.0034 0.000 13.0034 0.000 13.0034 0.000 13.0034 0.000 13.0034 0.000 13.0034 0.000 13.0034 0.000 13.0034 0.000 13.0034 0.000 13.0034 0.000 13.0034                                                                                                                                                                                           |                 |                     | 1 0.79   | 0.797    | 6960.4 | 0.000 |   |                |                     | 1    | 0.761  | 0.761  | 6342.2 | 0.000 |
| 3 0.442 0.002 3 0.400 0.044 11285. 0.000   4 0.346 0.010 1432. 0.000 4 0.311 0.023 12825. 0.000   6 0.226 0.019 15524. 0.000 6 0.192 0.056 13405. 0.000   7 0.185 0.000 6 0.147 0.006 139. 0.100 6 0.122. 0.000 9 0.120. 0.1359. 0.000 10 0.056 0.041 1359. 0.000 11 0.076. 0.066 13825. 0.000 10 0.056 0.041 1359. 0.000 11 0.056. 0.041 13559. 0.000 11 0.056. 0.041 13559. 0.000 11 0.056. 0.041 13559. 0.000 11 0.057. 13902. 0.000   12 0.042 0.001 1652. 0.000 13 0.034. 0.021 13921. 0.000                                                                                                                                                                                                                |                 |                     | 2 0.58   | 5 -0.145 | 10680. | 0.000 |   |                | 1 9                 | 2    | 0.540  | -0.094 | 9530.9 | 0.000 |
| 4 0.346 0.010 14132 0.000 5 0.276 0.244 0.006 1299 0.000   6 0.226 0.019 15524 0.000 6 0.124 0.006 1299 0.001 13058 0.000   7 0.185 0.001 1639 0.000 7 0.185 0.000 7 0.185 0.000 7 0.185 0.000 10 0.076 0.066 13222 0.000   9 0.120 0.012 16252 0.000 11 0.056 0.004 13856 0.000   11 0.076 0.001 16459 0.000 11 0.056 0.001 1302 0.042 0.031383 0.000   12 0.058 0.001 153 0.000 13 0.044 0.021 0.0313123 0.040 0.0313123 0.040 0.0313123 0.000 13 0.044 0.021 0.0315 0.020 0.01131320 0.000 13220                                                                                                                                                                                                              |                 | 1 7 1               | 3 0.44   | 0.072    | 12020. | 0.000 |   |                |                     | 3    | 0.400  | 0.054  | 11285. | 0.000 |
| 5 0.216 0.011 14552. 0.000 5 0.244 0.005 1293. 0.000   7 0.185 0.003 15898. 0.000 7 0.145 0.001 7 0.145 0.001 7 0.145 0.004 1365. 0.000   9 0.120 0.012 16232. 0.000 10 0.056 0.004 1385. 0.000   10 0.097 0.008 16495. 0.000 11 0.056 0.004 1380. 0.001 11 0.056 0.001 13 0.040 0.001 13 0.040 0.001 13 0.040 0.001 13 0.040 0.001 130 0.040 0.001 130 0.040 0.001 130 0.040 0.001 130 0.040 0.001 130 0.040 0.001 130 0.040 0.001 130 0.000 15 0.000 16 0.000 15 0.001 0.001 130                                                                                                                                                                                                                               |                 |                     | 6 0.34   | 0.010    | 14132. | 0.000 |   |                |                     | 1 2  | 0.311  | 0.023  | 12345. | 0.000 |
| 6 0.226 0.019 1524. 0.000 6 0.192 0.000 13405. 0.000   8 0.147 0.006 16398. 0.000 8 0.162 0.004 1355. 0.000   9 0.120 0.012 16292. 0.000 9 0.162 0.004 1355. 0.000   10 0.097 0.008 16395. 0.000 10 0.056 0.004 1355. 0.000   11 0.076 0.001 16459. 0.000 11 0.056 0.001 13883. 0.000   12 0.056 0.001 16452. 0.000 13 0.034 0.000 13812. 0.000   14 0.029 0.003 16522. 0.000 14 0.021 0.012 1392. 0.000   15 0.011 0.001 1522. 0.000 1393. 0.000 1393. 0.000   16 0.012 0.001 1522. 0.000 </th <th>-</th> <th></th> <th>6 0.20</th> <th>0.011</th> <th>14303.</th> <th>0.000</th> <th></th> <th></th> <th></th> <th>2</th> <th>0.244</th> <th>0.006</th> <th>12999.</th> <th>0.000</th>                         | -               |                     | 6 0.20   | 0.011    | 14303. | 0.000 |   |                |                     | 2    | 0.244  | 0.006  | 12999. | 0.000 |
| P 0.182 0.003 15995 0.000 P 0.145 0.014 1585 0.000   9 0.120 0.012 16232 0.000 9 0.076 0.006 13822 0.000   10 0.097 0.008 16395 0.000 10 0.056 0.004 13883 0.000   12 0.056 0.008 16495 0.000 12 0.042 0.005 13902 0.000   13 0.040 -0.007 16513 0.000 14 0.021 0.001 13902 0.000   14 0.029 0.003 16522 0.000 15 0.012 0.004 13921 0.000   16 0.004 16525 0.000 17 -0.007 0.012 13922 0.000   19 0.011 0.004 16525 0.000 17 -0.017 0.012 13924 0.000   21 -0.011 0.005 16525 0.000                                                                                                                                                                                                                              |                 |                     | 7 0 40   | 0.019    | 42000  | 0.000 |   |                |                     | 1 5  | 0.192  | 0.005  | 13405. | 0.000 |
| 6 0.147 0.000 18232 0.000 19 0.076 0.000 1332 0.000   10 0.097 0.008 16395 0.000 11 0.056 0.004 13855 0.000   12 0.058 0.008 16495 0.000 12 0.442 0.001 138.3 0.000   13 0.440 0.007 16513 0.000 12 0.422 0.005 13902 0.000   14 0.029 0.003 16622 0.000 14 0.021 0.913 13921 0.000   15 0.016 0.000 16525 0.000 17 0.007 13922 0.001   16 0.006 0.001 16525 0.000 17 0.007 0.012 13922 0.000   18 0.001 0.009 16525 0.000 19 0.020 13933 0.000   21 0.001 0.001 16525 0.000 22                                                                                                                                                                                                                                  |                 |                     | 9 0 14   | 0.003    | 16134  | 0.000 |   |                | 1 1                 | 1 4  | 0.145  | -0.014 | 13030. | 0.000 |
| 3 0.120 16395. 0.000 10 0.056 0.0001 13855. 0.000   11 0.076 0.001 16495. 0.000 11 0.056 0.0001 13835. 0.000   12 0.058 0.008 16495. 0.000 13 0.044 0.001 13835. 0.000   12 0.026 0.000 15 0.016 13902. 0.000   13 0.044 0.001 16513. 0.000 13 0.034 0.000 13915. 0.000   14 0.029 0.001 16525. 0.000 15 0.012 13922. 0.000   16 0.001 0.001 16525. 0.000 16 0.003 13935. 0.000   19 0.001 0.001 16525. 0.000 19 0.020 0.001 13934. 0.000   20 0.011 16525. 0.000 21 0.008 13933. 0.000 22 0                                                                                                                                                                                                                     |                 |                     | 0 0 12   | -0.000   | 10124. | 0.000 |   | 2              | 1 1                 | 1 2  | 0.105  | -0.004 | 13/59. | 0.000 |
| 11 0.037 0.000 11 0.058 0.004 13835 0.000   12 0.058 0.008 16495 0.000 12 0.042 0.001 13 0.001 13 0.001 13 0.034 0.000 13 0.034 0.000 13 0.034 0.000 14 0.022 0.000 14 0.021 0.015 1902 0.000   15 0.016 0.001 16525 0.000 15 0.012 13921 0.000   16 0.006 0.001 16525 0.000 17 0.007 0.012 13922 0.000   18 0.001 0.004 16525 0.000 18 0.012 0.001 3930 0.000   20 0.011 0.002 16525 0.000 19 0.020 0.018 3933 0.000   21 0.001 0.021 16525 0.000 21 0.008 0.011 3933 0.000 <t< th=""><th>5</th><th>1 I I</th><th>10 0.09</th><th>0.012</th><th>16395</th><th>0.000</th><th></th><th>1</th><th></th><th>1.3</th><th>0.076</th><th>-0.006</th><th>13022.</th><th>0.000</th></t<>                                 | 5               | 1 I I               | 10 0.09  | 0.012    | 16395  | 0.000 |   | 1              |                     | 1.3  | 0.076  | -0.006 | 13022. | 0.000 |
| 11 0.053 0.000 11 0.053 0.000   12 0.042 -0.005 13092 0.000   13 0.040 -0.007 16513 0.000 13 0.042 -0.005 13920 0.000   14 0.029 0.003 16522 0.000 14 0.021 0.041 13920 0.000   16 0.016 -0.017 16525 0.000 16 0.002 0.001 17 0.001 13920 0.000   17 0.001 0.001 16525 0.000 16 0.002 0.001 139320 0.000   18 0.001 0.000 16525 0.000 16 0.001 139330 0.000   20 0.014 0.002 16525 0.000 21 0.001 31334 0.000   21 -0.005 16525 0.000 22 0.001 0.001 13334 0.000   22 -0.001 16526                                                                                                                                                                                                                               |                 |                     | 11 0.07  | 5 .0 001 | 16459  | 0.000 |   |                | 1 I                 | 1.2  | 0.000  | 0.004  | 13000. | 0.000 |
| 12 0.032 0.000 12 0.032 0.000   13 0.034 0.000 1652.0.000 14 0.021.0.015 1392.0.000   14 0.029 0.003 1652.2.0.000 14 0.021.0.015 1392.0.000   15 0.016 0.001 1652.5.0.000 16 0.012.0.014 13921.0.000   17 0.001 0.004 16525.0.000 17.0.007.0.012 13922.0.000   19 0.001 0.009 16525.0.000 19.0.020 0.018 0.001   19 0.010 16525.0.000 19.0.020 0.018 0.003 13934.0.000   20 0.011 0.002 16525.0.000 21.0.006 0.011 13935.0.000   21 0.001 0.002 16525.0.000 21.0.006 0.011 13935.0.000   22 0.001 16525.0.000 21.0.006 0.011 13935.0.000   22 0.011 15252.0.000 21.0.006 0.011 13935.0.000   23 0.                                                                                                               |                 |                     | 12 0.05  | 10.000   | 16405  | 0.000 |   |                |                     | 1.4  | 0.050  | 0.013  | 13003. | 0.000 |
| 12 0.029 0.003 1652 0.000 13 0.001 13920 0.000   15 0.012 0.001 16525 0.000 15 0.012 0.001 13921 0.000   16 0.006 0.000 16525 0.000 16 0.007 0.012 13921 0.000   17 0.001 0.004 16525 0.000 17 0.007 0.012 13922 0.000   18 0.001 0.001 16525 0.000 18 0.019 0.002 13930 0.000   20 0.016 0.005 16525 0.000 21 0.008 0.013 3934 0.000   21 0.001 0.001 16525 0.000 21 0.008 0.013 3934 0.000   22 0.007 0.011 16525 0.000 21 0.008 0.013 3935 0.000   22 0.007 0.011 16525 0.000                                                                                                                                                                                                                                 |                 |                     | 13 0.04  | 0.007    | 16513  | 0.000 |   | 1              | I I .               | 12   | 0.042  | 0.005  | 13902. | 0.000 |
| 15 0.01 0.01 0.021 0.030 13201 0.000   16 0.016 0.001 16525 0.000 16 0.002 0.012 13221 0.000   16 0.001 0.001 16525 0.000 17 0.007 0.012 13222 0.000   17 0.001 0.001 16525 0.000 17 0.007 0.012 13920 0.000   19 0.001 0.000 16525 0.000 19 0.001 3930 0.000   20 0.014 0.005 16525 0.000 21 0.008 0.013 1334 0.000   21 0.001 0.002 16526 0.000 22 0.001 0.001 13334 0.000   22 0.007 0.011 16526 0.000 23 0.006 0.011 13334 0.000   23 0.012 16527 0.000 23 0.006 0.011 13335                                                                                                                                                                                                                                 |                 |                     | 14 0.02  | 0.003    | 16522  | 0.000 |   | 1              |                     | 14   | 0.034  | 0.000  | 13919. | 0.000 |
| 16 0.002 0.001 1552 0.000   17 0.001 0.004 16525 0.000 17 0.001 0.002 13921 0.000   18 0.001 0.004 16525 0.000 18 0.012 13922 0.000   19 0.020 0.001 16525 0.000 18 0.019 0.012 13926 0.000   20 0.001 0.005 16525 0.000 20 0.011 3934 0.000   21 0.001 0.005 16525 0.000 21 0.006 0.013 13934 0.000   22 0.001 0.002 16528 0.000 22 0.001 13934 0.000   23 0.012 0.002 16528 0.000 23 0.006 0.011 13935 0.000   24 0.019 0.0154 0.000 24 0.010 13938 0.000   25 0.015 0.056 <t< th=""><th>1</th><th></th><th>15 0.01</th><th>-0.017</th><th>16525</th><th>0.000</th><th></th><th>1</th><th>1 1</th><th>16</th><th>0.021</th><th>0.004</th><th>13920.</th><th>0.000</th></t<>                                    | 1               |                     | 15 0.01  | -0.017   | 16525  | 0.000 |   | 1              | 1 1                 | 16   | 0.021  | 0.004  | 13920. | 0.000 |
| 17 0.001 0.004 16525. 0.000 17 0.007 0.012 13922. 0.000   18 0.001 0.000 16525. 0.000 18 0.019 0.002 13920. 0.000   19 0.001 0.005 16525. 0.000 19 0.020 0.018 0.003 13930. 0.000   20 0.011 0.005 16525. 0.000 21 0.008 0.013 13934. 0.000   21 0.001 0.004 16526. 0.000 21 0.006 0.013 13934. 0.000   23 0.012 0.002 16526. 0.000 22 0.001 13935. 0.000   24 0.019 -0.015 16532. 0.000 24 0.010 0.011 13936. 0.000   25 0.027 0.003 16550. 0.000 26 0.013 3940. 0.000   26 0.015 16532. 0.000                                                                                                                                                                                                                  | 1               |                     | 16 0.00  | 0.000    | 16525  | 0.000 |   | 1              |                     | 16   | 0.003  | -0.012 | 13921  | 0.000 |
| 18 -0.001 0.000 16525. 0.000 18 -0.019 -0.012 13926. 0.000   19 0.001 0.009 16525. 0.000 19 -0.020 0.008 13930. 0.000   20 0.001 -0.005 16525. 0.000 20 -0.018 0.003 13934. 0.000   21 -0.001 -0.004 16525. 0.000 21 -0.008 0.019 13934. 0.000   22 -0.007 -0.011 16525. 0.000 21 -0.008 0.019 13934. 0.000   23 -0.012 -0.022 16528. 0.000 23 -0.006 0.011 13934. 0.000   24 -0.019 -0.015 16532. 0.000 23 -0.006 13935. 0.000   26 -0.031 -0.008 16562. 0.000 26 -0.015 13940. 0.000   29 -0.021 16578. 0.000 <                                                                                                                                                                                                |                 |                     | 17 0.00  | 0.004    | 16525  | 0.000 |   | 1              |                     | 17   | -0.007 | -0.012 | 13922  | 0.000 |
| 19 0.001 0.009 16525 0.000 19 0.020 0.008 13930 0.000   20 0.001 -0.005 16525 0.000 20 0.018 0.003 13934 0.000   21 -0.001 -0.004 16525 0.000 21 -0.008 0.019 13934 0.000   22 -0.001 -0.002 16526 0.000 22 -0.001 -0.001 13934 0.000   23 -0.012 -0.002 16526 0.000 23 -0.006 -0.011 13935 0.000   24 -0.019 -0.010 13935 0.000 24 -0.010 13936 0.000   25 -0.013 -0.001 1552 0.000 26 -0.013 -0.005 13940 0.000   26 -0.033 -0.008 16552 0.000 26 -0.015 -0.001 13935 0.000   29 -0.028 -0.002 16568                                                                                                                                                                                                           |                 |                     | 18 -0.00 | 0.000    | 16525  | 0.000 |   | 1              |                     | 1 18 | .0.019 | .0.012 | 13926  | 0.000 |
| 20 0.001 0.005 16525 0.000 20 0.018 0.003 13934 0.000   21 0.001 0.004 16525 0.000 21 0.008 0.019 13934 0.000   22 0.007 0.011 16525 0.000 22 0.001 13934 0.000   23 0.012 0.002 16525 0.000 22 0.001 13935 0.000   23 0.012 0.002 16525 0.000 24 0.010 0.001 13935 0.000   24 0.019 -0.015 16532 0.000 26 0.013 0.006 13935 0.000   26 0.033 0.008 16552 0.000 27 0.015 -0.005 13934 0.000   28 0.033 0.004 16562 0.000 29 -0.021 -0.003 13953 0.000   29 -0.021 0.002 16578 0.000 30                                                                                                                                                                                                                           |                 |                     | 19 0.00  | 0.009    | 16525  | 0.000 |   |                |                     | 19   | .0.020 | 0.008  | 13930  | 0.000 |
| $ \begin{array}{c ccccccccccccccccccccccccccccccccccc$                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                           | •               |                     | 20 0.00  | -0.005   | 16525. | 0.000 |   |                |                     | 20   | -0.018 | 0.003  | 13934  | 0.000 |
| $\begin{array}{cccccccccccccccccccccccccccccccccccc$                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                             |                 |                     | 21 -0.00 | -0.004   | 16525. | 0.000 |   | 1              |                     | 21   | -0.008 | 0.019  | 13934  | 0.000 |
| $ \begin{array}{c ccccccccccccccccccccccccccccccccccc$                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                           |                 |                     | 22 -0.00 | -0.011   | 16526. | 0.000 |   |                |                     | 22   | -0.001 | -0.001 | 13934. | 0.000 |
| 24 -0.019 -0.015 16532 0.000 24 -0.010 0.001 13936 0.000   25 -0.027 -0.009 16540 0.000 25 -0.013 -0.006 13938 0.000   26 -0.013 -0.006 16552 0.000 26 -0.015 -0.005 13938 0.000   27 -0.036 -0.004 16566 0.000 27 -0.019 -0.009 13944 0.000   28 -0.033 0.001 16578 0.000 29 -0.021 -0.003 13948 0.000   29 -0.022 16877 0.000 29 -0.021 -0.003 13958 0.000   30 -0.023 0.004 16592 0.000 31 -0.025 -0.021 13958 0.000   31 -0.019 -0.003 16600 0.000 32 -0.022 13956 0.000   32 -0.012 0.037 16603 0.000 <td></td> <td></td> <td>23 -0.01</td> <td>2 -0.002</td> <td>16528.</td> <td>0.000</td> <td></td> <td></td> <td></td> <td>23</td> <td>-0.006</td> <td>-0.018</td> <td>13935</td> <td>0.000</td>        |                 |                     | 23 -0.01 | 2 -0.002 | 16528. | 0.000 |   |                |                     | 23   | -0.006 | -0.018 | 13935  | 0.000 |
| $ \begin{array}{ c c c c c c c c c c c c c c c c c c c$                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                          |                 |                     | 24 -0.01 | 0.015    | 16532. | 0.000 |   |                |                     | 24   | -0.010 | 0.001  | 13936. | 0.000 |
| 26 -0.033 -0.008 16552 0.000 26 -0.015 -0.005 13940 0.000   27 -0.036 -0.004 16566 0.000 27 -0.019 -0.019 13944 0.000   28 -0.028 -0.021 16566 0.000 28 -0.021 0.001 13943 0.000   29 -0.028 -0.002 16587 0.000 29 -0.021 -0.003 13953 0.000   30 -0.023 0.004 16592 0.000 31 -0.026 -0.012 13966 0.000   31 -0.019 -0.003 16696 0.000 32 -0.021 13966 0.000   32 -0.017 -0.003 16603 0.000 32 -0.023 -0.014 13977 0.000   33 -0.017 -0.003 16605 0.000 33 -0.023 -0.014 13977 0.000   34 -0.012 0.013 16605<                                                                                                                                                                                                    | •               |                     | 25 -0.02 | 7 -0.009 | 16540. | 0.000 |   |                |                     | 25   | -0.013 | -0.006 | 13938  | 0.000 |
| 27 -0.036 -0.004 16566 0.000 27 -0.019 -0.009 13944 0.000   28 -0.033 0.010 16578 0.000 28 -0.020 0.011 13948 0.000   29 -0.021 -0.021 16578 0.000 29 -0.021 -0.003 13953 0.000   30 -0.023 0.004 16592 0.000 30 -0.021 -0.003 13958 0.000   31 -0.019 -0.003 16566 0.000 31 -0.022 -0.021 13956 0.000   32 -0.017 -0.003 16603 0.000 32 -0.023 0.011 13977 0.000   33 -0.017 -0.003 16605 0.000 33 -0.023 -0.011 13983 0.000   34 -0.012 0.013 16605 0.000 35 -0.023 -0.011 13983 0.000   36 0.009 0.003 <td>•</td> <td></td> <td>26 -0.03</td> <td>3 -0.008</td> <td>16552.</td> <td>0.000</td> <td></td> <td>i .</td> <td>1 1</td> <td>26</td> <td>-0.015</td> <td>-0.005</td> <td>13940.</td> <td>0.000</td> | •               |                     | 26 -0.03 | 3 -0.008 | 16552. | 0.000 |   | i .            | 1 1                 | 26   | -0.015 | -0.005 | 13940. | 0.000 |
| 28 -0.033 0.010 16578. 0.000 28 -0.020 0.001 13948. 0.000   29 -0.028 -0.002 16587. 0.000 29 -0.021 -0.003 13958. 0.000   30 -0.023 0.004 16592. 0.000 30 -0.021 -0.003 13958. 0.000   31 -0.019 -0.001 16596. 0.000 31 -0.026 -0.012 13966. 0.000   32 -0.018 -0.003 16603. 0.000 32 -0.023 -0.014 13977. 0.000   33 -0.017 -0.003 16605. 0.000 33 -0.023 -0.014 13977. 0.000   34 -0.012 0.013 16605. 0.000 34 -0.023 -0.014 13977. 0.000   35 0.009 0.003 16606. 0.000 36 -0.019 -0.004 13983. 0.000                                                                                                                                                                                                          | •               |                     | 27 -0.03 | 5 -0.004 | 16566. | 0.000 |   | •              |                     | 27   | -0.019 | -0.009 | 13944. | 0.000 |
| 29 -0.028 -0.002 1687. 0.000 29 -0.021 -0.003 13953. 0.000   30 -0.023 0.004 16592. 0.000 30 -0.021 -0.003 13958. 0.000   31 -0.019 -0.001 16592. 0.000 31 -0.026 -0.012 13966. 0.000   32 -0.018 -0.003 16600. 0.000 32 -0.023 0.012 13971. 0.000   33 -0.017 -0.003 16603. 0.000 33 -0.023 -0.014 13977. 0.000   34 -0.012 0.013 16605. 0.000 34 -0.023 -0.004 13983. 0.000   35 0.000 0.019 16605. 0.000 35 -0.020 0.004 13987. 0.000   36 0.009 0.003 16606. 0.000 36 -0.019 -0.006 13981. 0.000                                                                                                                                                                                                             | •               | 1 1                 | 28 -0.03 | 0.010    | 16578. | 0.000 |   |                |                     | 28   | -0.020 | 0.001  | 13948. | 0.000 |
| 30 -0.023 0.004 16592. 0.000 30 -0.021 0.003 13958. 0.000   31 -0.019 -0.001 16596. 0.000 31 -0.026 -0.012 13966. 0.000   32 -0.018 -0.003 16600. 0.000 32 -0.023 0.014 13971. 0.000   33 -0.017 -0.003 16603. 0.000 33 -0.023 -0.014 13977. 0.000   34 -0.012 0.013 16605. 0.000 34 -0.023 -0.014 13977. 0.000   36 0.009 0.003 16606. 0.000 36 -0.029 -0.004 13983. 0.000                                                                                                                                                                                                                                                                                                                                      | •               |                     | 29 -0.02 | 3 -0.002 | 16587. | 0.000 |   | •              | 1 1                 | 29   | -0.021 | -0.003 | 13953. | 0.000 |
| 31 -0.019 -0.001 16596.0.000 31 -0.026 -0.012 13966.0.000   32 -0.018 -0.003 16600.0.000 32 -0.023 0.012 13971.0.000   33 -0.017 -0.003 16603.0.000 33 -0.023 -0.014 13977.0.000   34 -0.012 0.013 16605.0.000 34 -0.023 -0.014 13977.0.000   36 0.009 0.003 16606.0.000 36 -0.029 0.004 13983.0.000   36 0.009 0.003 16606.0.000 36 -0.019 -0.006 13981.0.000                                                                                                                                                                                                                                                                                                                                                   | •               |                     | 30 -0.02 | 0.004    | 16592. | 0.000 |   | - +            |                     | 30   | -0.021 | -0.003 | 13958. | 0.000 |
| 32 -0.013 16600 .0.00 32 -0.023 0.012 13971 0.000   33 -0.017 -0.003 16603 0.000 33 -0.023 -0.014 13977 0.000   34 -0.012 0.013 16605 0.000 34 -0.023 -0.014 13977 0.000   35 0.000 0.019 16605 0.000 35 -0.020 0.004 13987 0.000   36 0.009 0.003 16606 0.000 36 -0.019 -0.006 13997 0.000                                                                                                                                                                                                                                                                                                                                                                                                                      | •               |                     | 31 -0.01 | 9 -0.001 | 16596. | 0.000 |   |                |                     | 31   | -0.026 | -0.012 | 13966. | 0.000 |
| 33 -0.017 -0.003 16603 0.000 33 -0.023 -0.014 13977 0.000   34 -0.012 0.013 16605 0.000 34 -0.023 -0.011 13983 0.000   35 0.000 0.019 16605 0.000 35 -0.020 0.004 13987 0.000   36 0.009 0.003 16606 0.000 36 -0.019 -0.006 13981 0.000                                                                                                                                                                                                                                                                                                                                                                                                                                                                          | 1               |                     | 32 -0.01 | 3 -0.003 | 16600. | 0.000 |   |                |                     | 32   | -0.023 | 0.012  | 13971. | 0.000 |
| 34 -0.012 0.013 16605. 0.000 34 -0.023 -0.001 13983. 0.000   35 0.000 0.019 16605. 0.000 35 -0.020 0.004 13987. 0.000   36 0.009 0.003 16606. 0.000 36 -0.019 -0.006 13991. 0.000                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                | 1               |                     | 33 -0.01 | -0.003   | 16603. | 0.000 |   |                |                     | 33   | -0.023 | -0.014 | 13977. | 0.000 |
| 35 0.000 0.019 16605. 0.000<br>36 0.009 0.003 16606. 0.000<br>36 0.019 -0.006 13991. 0.000                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                       | 1               |                     | 34 -0.01 | 2 0.013  | 16605. | 0.000 |   |                |                     | 34   | -0.023 | -0.001 | 13983. | 0.000 |
| 36 -0.019 -0.006 13991. 0.000                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                    | t               |                     | 35 0.00  | 0.019    | 16605. | 0.000 |   |                | I I I               | 35   | -0.020 | 0.004  | 13987. | 0.000 |
|                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                  | 4               | 1                   | 36 0.00  | 0.003    | 16606. | 0.000 |   | •              | 1 1                 | 36   | -0.019 | -0.006 | 13991. | 0.000 |

Autocorrelograms show significant partial autocorrelations at the order 3 (every partial autocorrelation at a superior order are inferior or equal to significativity threshold, equal to  $2/\sqrt{Sample \ size} = 0,019$ ). The AR3 model that has been developed in numerous papers (Cao & Wei, 2000; Tankov 2001; Roustant 2001; Barrieu 2002) is therefore retained. Its parameters are named 1, 2, 3.

- <u>Residual Rt modeling</u>

 $\sqrt{\sum_{k=4}^{N} (R_{t} - \phi_{1}R_{t-1} - \phi_{2}R_{t-2} - \phi_{3}R_{t-3})^{2}}$  minimum is computed (ordinary least squares fitting method) to estimate 1, 2, 3.

Following results have been obtained:

|   | Paris Montsouris | Bordeaux Mérignac |
|---|------------------|-------------------|
| 1 | 0,923            | 0,838             |

| 2 | -0,210 | -0,139 |
|---|--------|--------|
| 3 | 0,072  | 0,054  |

# <u>t residual of the AR(3)</u>

Diebold (2004) has suggested that residual seasonality is most often seasonal. To identify the seasonal component, residuals are modeled as follows:

 $_{t}$  =  $_{t}$   $_{t}$  where  $\sigma_{t}$  is AR residual volatility, supposed strictly positive, non constant in time.

Squaring this expression, then raising it to logarithm, the following result is obtained:

 $\ln(t^{2})=2.\ln(t^{2})+\ln(t^{2})$ 

In( $t^2$ ) is supposed not seasonal. In( $t^2$ ) periodogram is therefore computed.

# For Paris Montsouris:



# For Bordeaux Mérignac :



A yearly and half-yearly periodicity for t can be inferred.

t is modeled by  $_0$  + a cos(2 t/365)+ b sin(2 t/365)+ c cos(4 t/365)+ d sin(4 t/365).

Modeling parameters are estimated minimizing  $\ln(t^2)^2$  which is likelihood logarithm. Following results are obtained:

|   | Paris Montsouris | Bordeaux Mérignac |
|---|------------------|-------------------|
| 0 | 1,058            | 1,117             |
| а | 0,031            | 0,152             |
| b | 0,075            | 0,019             |
| С | 0,066            | 0,084             |
| d | -0,037           | -0,047            |

AR3 parameters are then computed again to minimize t

|   | Paris Mo        | ontsouris        | Bordeaux Mérignac |                  |  |  |  |  |  |
|---|-----------------|------------------|-------------------|------------------|--|--|--|--|--|
|   | After iteration | Before iteration | After itération   | Before itération |  |  |  |  |  |
| 1 | 0,919 (-0,4%)   | 0,923            | 0,838 (+0,03%)    | 0,838            |  |  |  |  |  |
| 2 | -0,208 (+1,0%)  | -0,210           | -0,145 (-4,3%)    | -0,139           |  |  |  |  |  |
| 3 | 0,072 (+0,3%)   | 0,072            | 0,057 (+4,7%)     | 0,054            |  |  |  |  |  |

The resulting noise presents satisfactory characteristics:

- it doesn't present significant autocorrelation,
- it doesn't present significant seasonality,
- it seems stationary,
- its 3<sup>rd</sup> and 4<sup>th</sup> order moments are close from being Gaussian, even though Jarque Bera test doesn't conclude this kind of modeling should be considered.

This noise will therefore be generated numerically, using its inverse repartition function.

Temperature has been modeled on 1988-2003 period as presented below:

 $T_t = Trend_t + Seas_t + R_t$  with

 $_{\rm t}$  a noise numerically generated from its inverse repartition function.

# IV.2. Pay-off estimation of weather derivatives considered

Following notations are proposed: weather derivatives corresponding to  $1^{er}$  of July to 30 September will be called "long" products, and weather derivatives corresponding to  $1^{er}$  of August to 15 August will be called "short" products. Corresponding premium P can be simply computed using following expression: P = E[pay-off] +  $\tilde{}$  [pay-off], with the seller risk aversion parameter.

A viticulturist that wishes to use weather derivatives would express his need as: « I wish a pay-off superior or equal to X for a risk level that occurs 20% or 30% of years (what he would consider as "bad seasons" from a climatic point of view), and to pay the smallest premium ».

Following notations are proposed (taking the case of a pay-off fixed for 30% of years):

- CDD Cooling Degree Days,
- U the "underlying" (corresponding to Cooling Degree Days sum on the period, in °C.days),
- $U_{30\%}$  the underlying level verifying Prob(U<U<sub>30\%</sub>)=30\%,
- U<sub>sup</sub> the strike for the "long" product,
- t the tick,

Viticulturist request (for the "long" product) corresponds to the search for  $U_{sup}$  minimizing premium under the constraint of a pay-off at  $U_{30\%}$  equal to X, which means to search for  $U_{sup}$  minimizing (E[max( $U_{sup}$ -U; 0)]+  $\tilde{[max(U_{sup}-U; 0)]}$ ).t under the constraint

 $(U_{sup}-U_{30\%}).t = X.$ 

Answer viticulturist request would therefore consist in determining:

$$U_{sup} \text{ minimizing } \frac{E\left[\max(U_{sup} - U; 0)\right] + \lambda . \sigma \left[\max(U_{sup} - U; 0)\right]}{U_{sup} - U_{30\%}}$$

To determine  $U_{sup}$  of the product corresponding to viticulturist request, it is therefore necessary to identify  $U_{30\%}$  with a sufficient precision.

To do so, 1000 yearly temperature series are computed for Paris and Bordeaux using the above temperature model. For each of these series, underlying U is computed. Underlying U distribution can be numerically estimated from these series, and is represented below for each of considered products. Weather derivatives pay-off described in chapter II can be inferred fixing strike and tick t. Corresponding premiums could also be computed fixing risk aversion parameter .







So, for Bordeaux "long" product,  $U_{30\%} = 355^{\circ}$ C/days and  $U_{40\%} = 367^{\circ}$ C/days. This highlights the accuracy need for temperature modeling to correctly price these products: between those two values, deviation is only 12°C/days for a 3 months period. Mean daily temperature bias must therefore be inferior to 0,375°C (~ 0,675°F) to offer a risk cover precise by ± 10 %.

This is on the same scale as non stationarity identified in chapter IV.1.3.1. To price with a precision better than  $\pm$  10 %, it seems necessary to refine trend modeling. These graphs highlight also significant differences between Paris and Bordeaux:

- The abscissas are shifted, which reflects the gap between those two cities gap.
- Underlying distribution of the "long" product is strongly asymmetrical, due to the 18°C threshold, reached much more often in Paris than in Bordeaux in July and in September.



Temperature series also allow the computing of expected value and standard deviation of the pay-off, function of the strike, and therefore, of the premium.

This highlights several major differences between Bordeaux and Paris:

- Curbs are shifted by the mean temperature gap between those two towns (graphs scales have also been shifted to simplify comparison);
- Standard deviation is higher for Bordeaux, which can rise the cost of these products, particularly if risk aversion parameters are high;
- Differences on "long" product due to higher impact of the threshold of 18°C on Paris CDD are found again: pay-off expected value is truncated for the first values of the strike.

Even before the study of the correlation between Paris and Bordeaux temperatures, these differences are important enough to conclude that two identical products, one based on Paris temperatures and the other on Bordeaux temperatures, would present a significant price gap.

### V. DISCUSSION AND IMPLICATION

Given the technical issues concerning the pricing of weather derivatives, it cannot be proposed as such to viticulturists. Two ways of implementation can be foreseen :

- To turn to brokers to market these products. Indeed, they can deliver some of the necessary communication and formation to viticulturists. On the other hand, they will generate additional transaction costs.
- These products can be used by insurance companies as an alternative solution to reinsurance. These products allow the transfer of some of the price and the volume risks to a more liquid energy market. They are therefore useful products for companies proposing crop and revenue insurance.

To validate this approach, a study should be lead with viticulturists to confirm the choice of the weather risks covered. Two comparaisons should also be lead :

- between the pay-off and viticulturists revenue,
- between the pay-off and crop and revenue insurance indemnisation.

A complete pricing, including management costs, should then be defined for specific areas. A first business model of the product could then be realised, and confronted to a panel of viticulturists and of insurance companies.

On the basis of a study on the weather-related risks viticulturists have to face, suitable products for the management of these risks have been proposed. Temperatures of Paris and Bordeaux have been carefully modeled so as to propose a method allowing the set up of a pricing. Compared to the latest published papers, gains of precision were sought by developing several elements. Determinist part has been refined proposing an empirical criterion to identify the trend breakpoint, and to estimate seasonal and trend parameters through two iterations. Stochastic parameters were estimated using generalized least squares fitting method, which has brought an increase of autoregressive model accuracy. Finally, instead of estimating residual noise using a Gaussian or hyperbolic distribution, a numerical estimation based on the inverse repartition function.

From this study, several research paths can be foreseen.

First, climate modelisation can be further improved. Concerning determinist modeling, climate physical modeling results may be used, particularly to define the trend. Besides, this paper is not tackling the issue of correlation between temperature risks measured at Bordeaux Merignac meteorological station, and risks actually concerning such or such vineyard in the area. To better estimate derivative products adaptation, this hypothesis could be studied comparing Bordeaux temperatures series, and temperatures series measured directly on vineyards. This kind of research can be lead using mini-meteorological station on field that allow experts to infer relationships between the two temperature series.

Another research path would be to correlate several cities temperatures to confirm the necessity of designing local products.

The study of pluviometry-related risks, and their correlation with temperature risks, could be a major supplement to this paper.

Secondly, to better evaluate the attractivness of the product, correlation between climate and either viticulturists revenues or insurance indemnisation can be further modelised.

Finally, a behavioral study could complete the understanding of how viticulturists would use this kind of products.

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